



A finite-element method framework for modeling rotating machines with superconducting windings

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KIT-CENTRE ENERGY



A hybrid model





Source: Toyota



Motivation

- Build a "do-it-all" dynamical model for electrical machines with superconducting winding
 - Simulate the whole geometry
 - Calculate AC losses in superconducting winding
 - Implement the model in a widely used platform \rightarrow Comsol Multiphysics
- Main idea: divide the (2D) geometry in two different parts:
 - One part for conventional material, the other for superconductors
 - Exploit the best formulation of Maxwell's equations for each part:
 - A-formulation for conventional materials
 - H-formulation for superconductors

Main issue: how to join the two parts?

Before continuing: why two formulations?



A couple of observations:

- The FEM simulation of flux dynamics in superconductors characterized a power-law <u>seems</u> to be more reliable with the *H*-formulation than with the *A*-formulation*
- The conditions of continuity of the physical quantities between the rotating and the fixed parts are more easily obtained with the continuity of a scalar quantity (the potential A in 2D) than with a vector one (the H field components).

*For the record: A-formulation models have been developed both with commercial¹ and home-made² codes.

¹ Nibbio et al 2001 IEEE TAS **11** 1 2631 ² Lathinen et al 2012 SuST **25** 11 115001

The power-law and the formulations



- Equivalent algebraic forms of the E-J power law
- (1) $\rho(J) = \rho_0 |J/J_c|^{n-1}$ (2) $\sigma(J) = \sigma_0 |J/J_c|^{1-n}$ (3) $\rho(E) = \rho_0 |E/E_c|^{1-1/n}$ (4) $\sigma(E) = \sigma_0 |E/E_c|^{1/n-1}$
- In the model implementation, circular definitions must be avoided
 A-formulation:
 - $\sigma(E)\partial_t A \frac{1}{\mu}\nabla^2 A = J_e \qquad \qquad B = \nabla \times A, \qquad E = -\partial_t A, \\ J = \sigma(E)E + J_e$
- E is a primary quantity \rightarrow (4) can be used

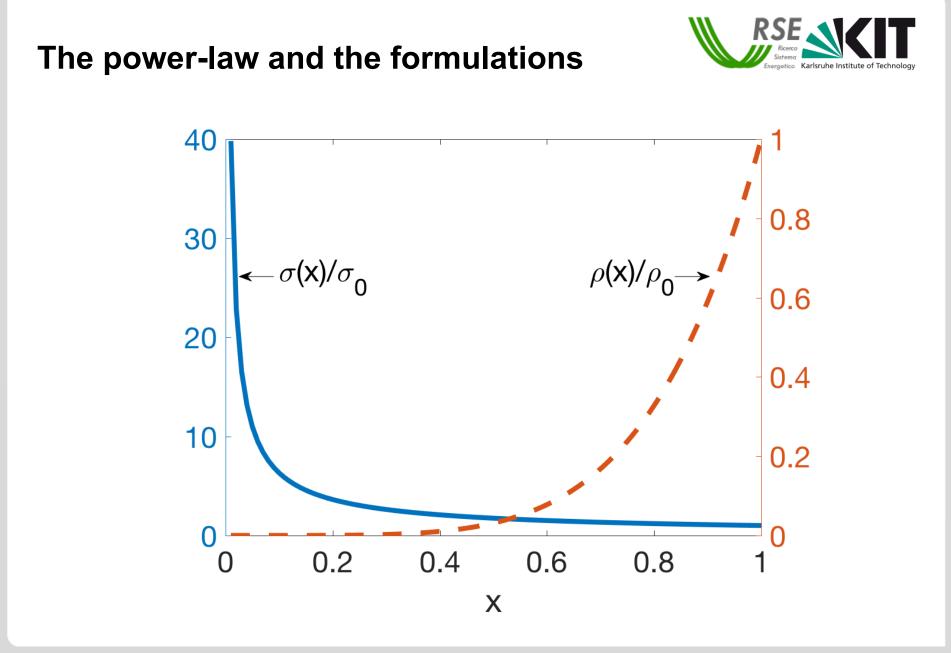
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- In the model implementation, circular definitions must be avoided
 H-formulation:

 $\mu \partial_{t} \boldsymbol{H} + \nabla \times \boldsymbol{E} = 0 \qquad \boldsymbol{J} = \nabla \times \boldsymbol{H}, \qquad \boldsymbol{E} = \rho(\boldsymbol{J}) \boldsymbol{J}$

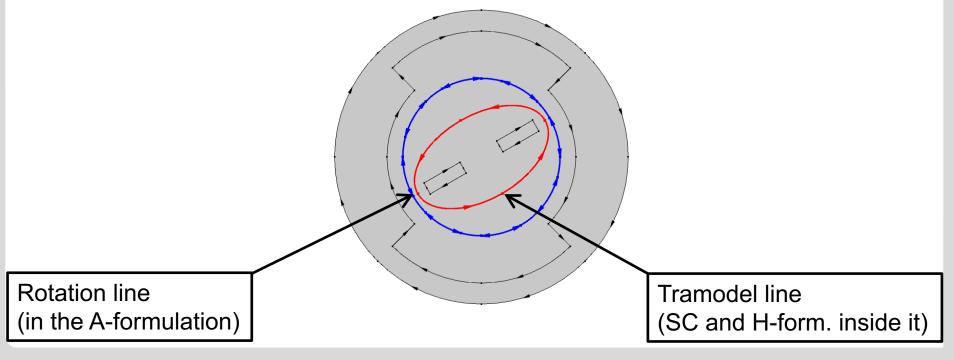
J is a primary quantity \rightarrow (1) can be used



Two important lines



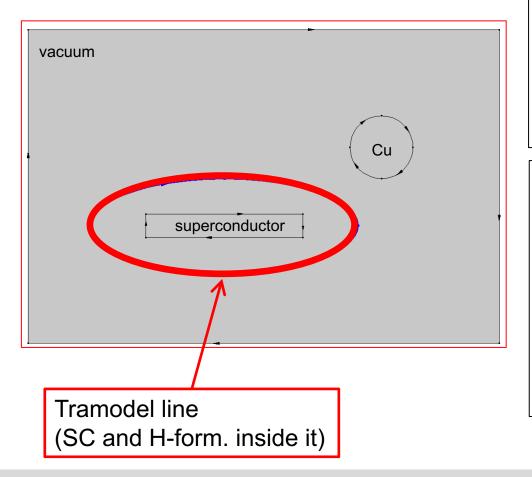
- **Tramodel** line: separates the *A* and *H*-formulation parts
- Rotation line: separates the rotating and fixed parts
- In 2D, A is a scalar \rightarrow Ideal solution:
 - Divide the geometry so that the rotation line is inside the *A*-formulation part
 - Scalar continuity between two (rotating/fixed) coordinate systems



Coupling the A- and H-formulation parts



Rectangular superconductor and round Cu wire carrying opposite currents



Current definitions

$$I_{SC} = \int_{SC} J_z(t) ds = I_a(t)$$
$$J_e(t) = \sigma V_{wire}(t)/L$$

Setting tangential components of the magnetic field equal

$$H_{t}^{(A)} = t_{x} \cdot H_{x} + t_{y} \cdot H_{y}$$
$$H_{t}^{(H)} = t_{x} \cdot H + t_{y} \cdot K$$
$$H_{t}^{(H)} = H_{t}^{(A)}$$

Ineffective!!!

Coupling the A- and H-formulation parts

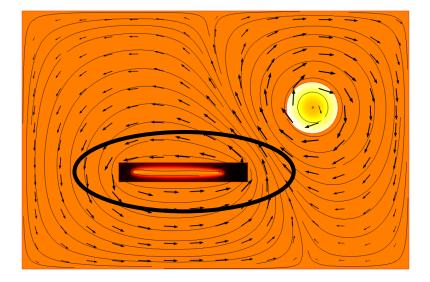


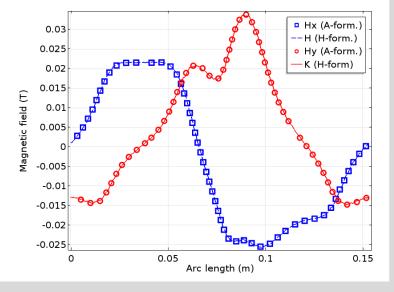
- In Comsol, coupling conditions are effective if we add two Weak Contribution instructions on the tramodel line:
 - A-formulation $H_t \cdot \text{test}(A_z)$
 - *H*-formulation $E_z \cdot \text{test}(H_t)$

This forces the common values as sources:

• $H_t^{(H)}$ acts as a source for the A-formulation part

 $\partial_t A_z = E_z \text{ acts as a source for the } H \text{-formulation part}$





Effective!!!

Francesco Grilli KIT-ITEP

6th International Worskhop on Numerical Modelling of HTS - Caparica, Portugal, 26-29 June 2018

Application to rotating systems



- Two reference systems
 - Fixed part (spatial frame) \rightarrow (x, y)
 - Rotating part (material frame) \rightarrow (*X*, *Y*)
- Link between temporal coordinates

$$\begin{pmatrix} X(x, y, t) \\ Y(x, y, t) \end{pmatrix} = T \begin{pmatrix} x \\ y \end{pmatrix} \qquad \qquad T = \begin{pmatrix} \cos(\omega t) & \sin(\omega t) \\ -\sin(\omega t) & \cos(\omega t) \end{pmatrix}$$

The vectors undergo a similar transformation

$$\binom{B_X}{B_Y} = T\binom{B_X}{B_y}$$

Application to rotating systems



- Field equations solved in both reference systems
- What is the transformation of physical quantities from one reference system to the other one?

 $\boldsymbol{B}_{\text{spatial}}(x, y) = \boldsymbol{B}_{\text{material}}(X, Y)$

 $\boldsymbol{E}_{\text{spatial}}(x, y) = \boldsymbol{E}_{\text{material}}(X, Y) - \boldsymbol{\nu}(x, y) \times \boldsymbol{B}_{\text{material}}(X, Y)$

v(*x*, *y*) velocity of a point of the rotor in the spatial frame
 v = (*v_x*, *v_x*, 0) = *ω*×*x* = (-*ωy*, *ωx*, 0)
 In the 2D case, we will have:

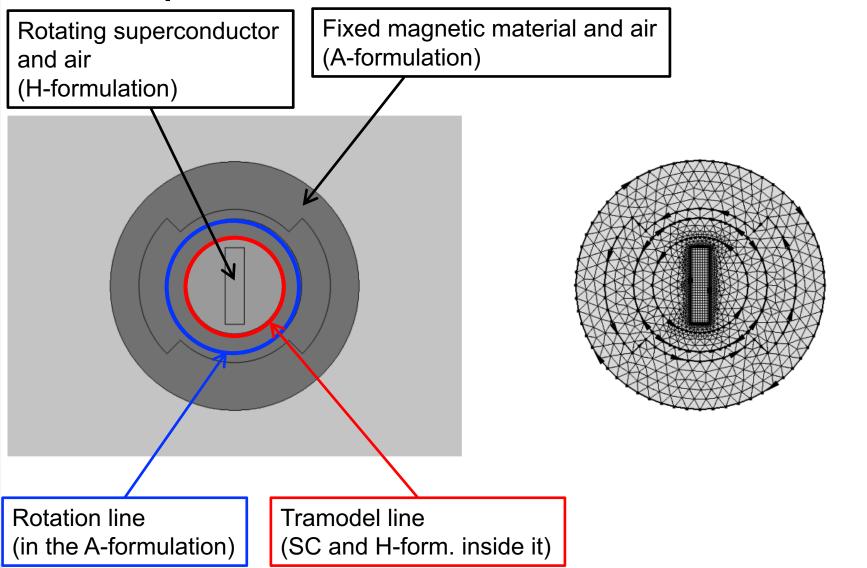
$$\begin{pmatrix} B_X \\ B_Y \end{pmatrix} = T^{-1} \begin{pmatrix} B_X \\ B_Y \end{pmatrix} \qquad \qquad E_z = E_Z + \omega (XB_X + YB_Y) = E_Z + dE_Z$$

In passing from one reference system to the other:

- The magnetic field simply rotates
- The electric field rotates and changes its magnitude

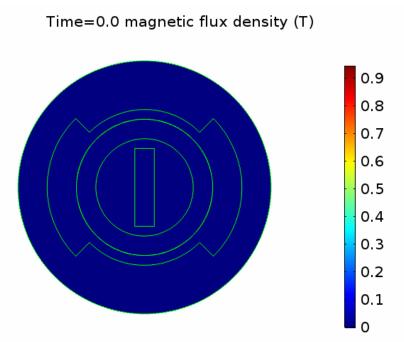
An example



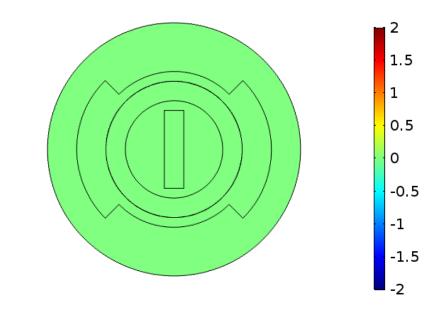


An example





Time=0.0 normalized current density J/Jc



Conclusion



- New FEM framework for modeling electrical machines employing superconductors:
 - H-formulation for regions containing superconductors
 - A-formulation for the rest
- Electromagnetic quantities joined on the line separating the two formulations ("tramodel" line) by means of weak contribution boundary conditions
- Tramodel line can be in the rotating or fixed part → joining conditions different in the two cases

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The model will be freely available on

http://www.htsmodelling.com/



Source: Toyota

Just to be clear: **not** the car model!!!

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Thank you very much for your attention!

Muito obrigado pela vossa atenção!